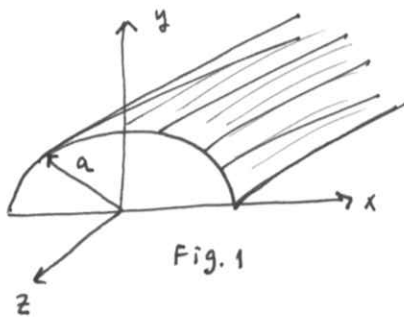


- ① A circular waveguide of radius,  $a$ , 3 cm that is filled with polystyrene ( $\epsilon_r = 2.56$ ) is used at a frequency of 2 GHz. For the dominant  $TE_{m,n}$  mode, determine the followings:

(a) Cut-off frequency, (b) Guided wavelength (cm), (c) phase constant,  $k_z$ , (rad/cm), (d) wave impedance

- ② The TE modes of a waveguide can be derived by letting the vector potentials  $\vec{A}$  and  $\vec{F}$  be equal to  $\vec{A} = 0$  and  $\vec{F} = \hat{a}_z F_z$ . The vector potential  $\vec{F}$  must satisfy the vector wave equation which reduces to  $\nabla^2 F_z + k^2 F_z = 0$  for  $\vec{F} = \hat{a}_z F_z$ . Consider a half-circle-shaped cross section for a



circular waveguide shown in Fig. 1. The radius of the half circle is 'a'. If one assumes that waves propagate only in the  $+z$  direction (assume an  $\infty$  long waveguide), the solution for

$$F_z^+ \text{ is of the form } F_z^+ = [A_1 J_n(\beta_r r) + B_1 Y_n(\beta_r r)] [C_2 \cos(n\theta) + D_2 \sin(n\theta)] e^{-j\beta_z z}$$

with  $\beta_z^2 + \beta_r^2 = k^2$ , which is a solution to  $(\nabla^2 + k^2) F_z = 0$  in cylindrical coordinates. Derive simplified expressions for the vector potential

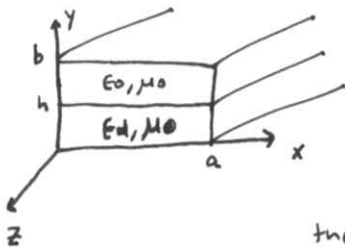
component, electric and magnetic fields and the cut-off frequencies for TE modes.

Hint: Use  $\vec{E} = -\frac{1}{\epsilon} \nabla \times \vec{F}$  and  $\vec{H} = -j\omega \vec{F} - \frac{j}{\omega \mu \epsilon} \nabla(\nabla \cdot \vec{F})$

Bonus PART for question ②: For problem ② Once the vector potential  $\vec{F}$  is found,  $\vec{H}$  can be found using either  $\vec{H} = -j\omega \vec{F} - \frac{j}{\omega \mu \epsilon} \nabla(\nabla \cdot \vec{F})$  or  $\vec{H} = \frac{-1}{j\omega \mu} \nabla \times \vec{E}$  with  $\vec{E} = -\frac{1}{\epsilon} \nabla \times \vec{F}$ .

However, at a first glance the resultant  $\vec{H}$  fields seem different. Show that  $\vec{H}$  fields found using either formulation is correct and they are identical.

- ③ Consider the geometry of the partially dielectric loaded rectangular waveguide shown in Fig. 2. For such a structure (i.e., this one and similar ones) TE modes can not satisfy the boundary conditions and hence, a combination of them, so called longitudinal section electric (LSE) or longitudinal section magnetic (LSM) modes, are used. For TE modes (i.e., LSE or TE or  $H_z$  modes), assume that the structure is infinitely long along the  $z$ -axis and we have only  $\pm z$  travelling waves. To analyze such a geometry, follow the procedure given below and answer the questions asked at each item.



- (a) Assume  $\vec{F} = F_y^+(x, y, z) \hat{a}_y$  and  $\vec{A} = 0$ , and solve the Helmholtz equation for  $F_y$  in both regions: namely, one for the dielectric region ( $0 \leq x \leq a$ ,  $0 \leq y \leq h$ ,  $z$ ) and the other for the free-space region ( $0 \leq x \leq a$ ,  $h \leq y \leq b$ ,  $z$ ).

(b) Find the field expressions from  $\vec{E} = -\frac{1}{\epsilon} \nabla \times \vec{F}$  &  $\vec{H} = -j\omega \vec{F} - \frac{j}{\omega \mu \epsilon} \nabla(\nabla \cdot \vec{F})$

(c) Apply all boundary conditions and obtain all necessary constants, etc.

(d) Finally, obtain the two transcendental equations.